

Why Hollow Sections?



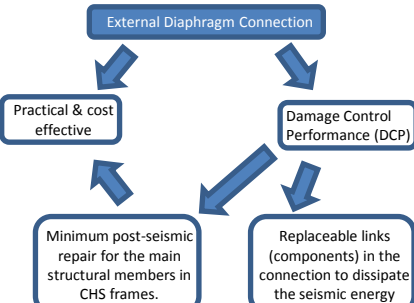
- Better strength to weight ratio
- Aesthetically pleasing
- Wide and diverse applications

BUT these advantages are often under-exploited due to:

- The perceived difficulties on cost effective connections between I-beams and hollow section columns.
- Relative lack of design guidance and of experimental data related with the cyclic inelastic behaviour of these connections.

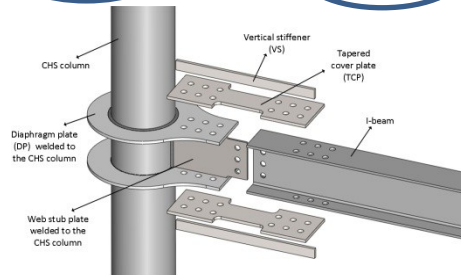
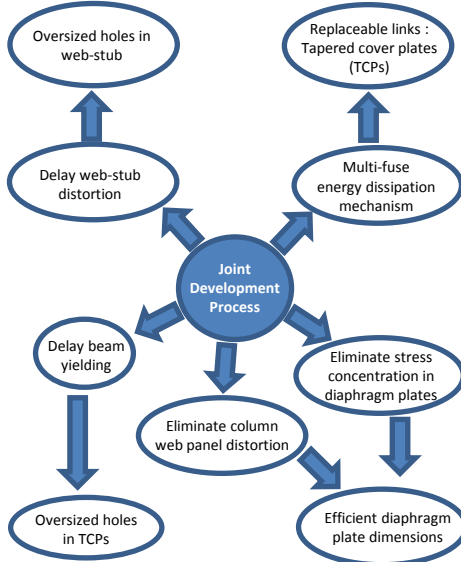
Aims and Objectives

- Design a cost effective connection between steel I-beam and circular hollow section (CHS) column.



- Determine the hysteretic (energy dissipative) behaviour of the external diaphragm connection type by full scale laboratory tests.
- Calibrate the non-linear finite element models (ABAQUS) against experimental results for parametric analyses on key geometric parameters with an aim of achieving optimum design arrangement.
- Derive design expressions in line with CIDECT design guide and Eurocode 3 Part 1-8 (CEN 2005) which will be calibrated against experimental data in accordance with Eurocode 0 (CEN 2002).

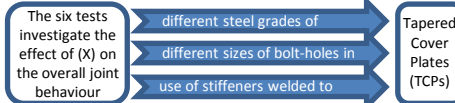
Development of The Joint Design



General view of the components of I-beam to CHS joint

Experimental Progress

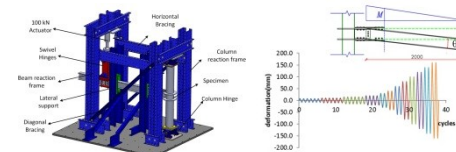
Six laboratory tests are conducted for the proposed connection to investigate its hysteretic behaviour. All tests have the same exact specimen and differ only in the type of tapered cover plates employed to connect the diaphragm plates to the I-beam flanges.



The components of each test specimen are:

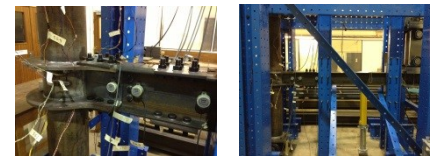
Component	Steel Grade	Geometry
CHS	S355	244X10mm Length = 2000mm
I-beam	S355	UB 203X133X30 Length = 2000mm
2 x Diaphragm Collar Plates	S355	Ring width = 90mm Thickness = 15mm
Web Stub	S355	Thickness = 8mm Oversized holes (16+6mm)
2 x Tapered Cover Plates (TCPs)*	S235 or S355*	Thickness = 12mm Normal holes (22mm) or oversized (22+6mm)*
2 x Vertical Stiffeners (VSs)*	S235 or S355*	Height = 40mm Thickness = 12mm

* TCPs and VSs are different for every test

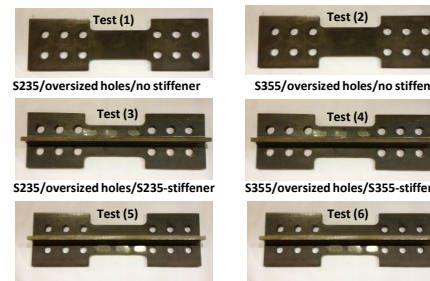


General layout of the test arrangement

Loading protocol based on AISC



Photographs of the test specimen

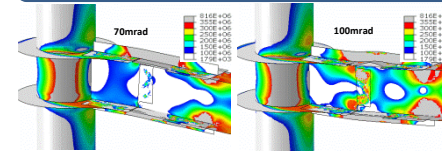


S235/normal holes/S235-stiffener S355/normal holes/S355-stiffener

Types of TCPs used in laboratory experiments

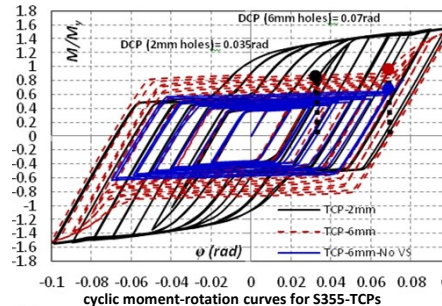
Experimental results for the six proposed tests will be reported in near future.

Finite Element Analysis

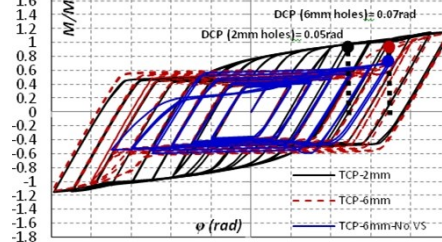


Von-Mises stress distribution for the connection FE model in ABAQUS (TCPs with stiffeners and oversized holes)

- Failure occurs in TCP at 100mmrad rotation.
- web distortion is delayed till 70mmrad rotation.



-0.1 -0.08 -0.06 -0.04 -0.02 0 0.02 0.04 0.06 0.08 0.1



-0.1 -0.08 -0.06 -0.04 -0.02 0 0.02 0.04 0.06 0.08 0.1

cyclic moment-rotation curves for S235-TCPs

Conclusions

- Multi-fuse energy mechanism is created and failure occurs in the replaceable link of the connection (TCPs).
- The VSs delay buckling of TCPs and improve the moment-rotation behaviour.
- The oversized holes in the web connection delay web distortion.
- Oversize holes in TCPs increase the DCP rotation limit.
- Reduced TCP/VS steel grades increase the DCP rotation limit.

Acknowledgement

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